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# LINEAR SAMPLED SYSTEM WITH TIME DELAY WHICH IS A FRACTION OF THE SAMPLING PERIOD

K. J. ÅSTRÖM

REPORT 7217 (B) AUGUST 1972 LUND INSTITUTE OF TECHNOLOGY DIVISION OF AUTOMATIC CONTROL LINEAR SAMPLED SYSTEM WITH TIME DELAY WHICH IS A FRACTION OF THE SAMPLING PERIOD

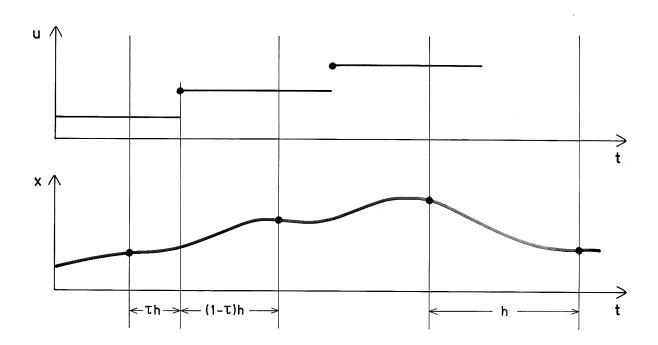
K.J. Åström

### Abstract

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$$\frac{dx}{dt} = Ax(t) + Bu(t-\tau h)$$

Assume that the input signal is kept constant over sampling intervals of length h. The input u and the state x is illustrated in Fig. 1.



## Fig. 1.

The value of the state vector at the sampling points is then given by

$$x(t+h) = \Phi x(t) + \Gamma_1 u(t) + \Gamma_2 u(t-h)$$
 (1)

where

$$\Phi = e^{Ah}$$
 (2)

$$\Gamma_1 = \int_0^{h(1-\tau)} e^{As} Bds \tag{3}$$

$$\Gamma_2 = \int_{h(1-\tau)}^{h} e^{As} Bds \tag{4}$$

Notice that

$$\Gamma_1 + \Gamma_2 = \int_0^h e^{As}$$
 Bds

The only difference compared to the usual case is thus that the term u(t-h) appears in (1).

The puls transfer function relating the state to the input is thus given by

$$H(z) = \left[zI - \Phi\right]^{-1} \left[\Gamma_1 + z^{-1}\Gamma_2\right] \tag{6}$$

## Single Input Single Output Systems

In the single-input single-output case we choose the coordinates in the state space representation so that the matrix  $\Phi$  is a companion matrix i.e.

$$\Phi = \begin{bmatrix} -a_1 & 1 & 0 & \dots & 0 \\ -a_2 & 0 & 1 & \dots & 0 \\ \vdots & & & & & \\ -a_{n-1} & 0 & 0 & \dots & 1 \\ -a_n & 0 & 0 & \dots & 0 \end{bmatrix}$$
(7)

Furthermore denote

$$\Gamma_{1} = \begin{bmatrix} \gamma_{1} \\ \gamma_{2} \\ \vdots \\ \gamma_{n} \\ \end{bmatrix}, \quad \Gamma_{2} = \begin{bmatrix} \gamma_{1} \\ \gamma_{2} \\ \vdots \\ \gamma_{n} \\ \end{bmatrix}$$
(8)

If the output y is chosen as the first component of the state-vector i.e.  $y=x_1$  we thus find that the input output relation is given by

$$y(t) + a_1 y(t-1) + \dots + a_n y(t-n) = \gamma_1^1 u(t-1) + (\gamma_2^1 + \gamma_1^2) u(t-2) + \dots + (\gamma_n^1 + \gamma_{n-1}^2) u(t-n) + \gamma_n^2 u(t-n-1)$$
(9)

which is identical to the standard form

$$A(q)y(t) = B(q)u(t-1)$$
 (10)

where the polynomials A and B are both of degree n. Notice that in the case when the timedelay is an integer multiple of the sampling interval the polynomial B in (10) is of degree n-1.

A consequence of importance for system identification is thus that it is reasonable to consider models where the polynomials A and B are of the same degree as the standard case. It is also clear that the model (9) can be used as a basis for adaptive algorithms that can handle variable time delays.

## An Example

As an illustration we Will consider the first order system

$$\dot{x}(t) = -x(t) + u(t-\tau h)$$

It is assumed that the input u is kept constant over sampling intervals of length h, we thus find that the values of the state variable at the sampling intervals are given by (1) where

$$\phi = e^{-h} = a$$

$$\Gamma_1 = 1 - e^{-h(1 - \tau)} = b_1$$

$$\Gamma_2 = e^{-h(1 - \tau)} - e^{-h} = b_2$$

The transfer function of the system is thus given by

$$H(z) = \frac{b_1 + b_2 z^{-1}}{z + a}$$

Notice that the pulse transfer function has a zero

$$z = -\frac{b_2}{b_1} = -\frac{1 - e^{-h(1-\tau)}}{e^{-h(1-\tau)} - e^{-h}}$$

which is outside the unit circle if

$$\tau > 1 + \frac{1}{n} \log \frac{1 + e^{-h}}{2} = f(h)$$

A graph of the function f is shown in Fig 2.

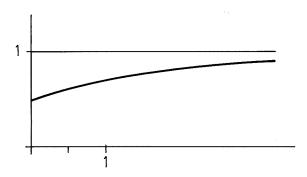


Fig. 2
Graph of  $f(x) = 1 + \frac{1}{x} \log \frac{1+e^{-x}}{2}$ 

The sampled system will thus be nonminimum phase if the delay  $\tau$  is sufficiently large. The critical value of  $\tau$  depends on the sampling interval. Notice that if  $\tau$  < 0.5 the zero of the pulse transfer function is always inside the unit circle.

#### 3. REFERENCE

Bolam, F. "Papermaking Systems and their Control" Trans of the Symposium held in Oxford Sept 1969. The British Paper and Board Maker's Association, London 1970.